

Linear power flow model

Samuel Talkington
Georgia Tech ECE

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Problem setup

Notation

- $j := \sqrt{-1}$
- $I_{n \times n}$ $n \times n$ identity matrix
- $\mathbf{1}_n$ n -dimensional vector of all ones
- $\mathbf{w} := [w_{ij}]_{(i,j) \in \mathcal{E}}$ network parameters; graph edge weights
- $\mathbf{A} \in \{0, \pm 1\}^{m \times n}$ edge-to-node incidence matrix
- $\text{diag}(\cdot)$ diagonal matrix with the argument as entries
- $\{\cdot\} \circ \{\cdot\}$ elementwise multiplication of two vectors.

Admittance matrix

The *admittance matrix* $\mathbf{Y} := \mathbf{G} + \mathrm{j}\mathbf{B} \in \mathbb{C}^{n \times n}$ is a generalization of the *weighted graph Laplacian matrix*. It is a complex, symmetric, but *not necessarily Hermitian* matrix, and its entries take the form

$$Y_{ik} = \begin{cases} w_{ii} + \sum_{l \neq i} w_{il} & i = k \\ -w_{ik} & \text{otherwise,} \end{cases} \quad (1)$$

or equivalently,

$$G_{ik} + \mathrm{j}B_{ik} = \begin{cases} \left(g_{ii} + \sum_{l \neq i} g_{il}\right) + \mathrm{j} \left(b_{ii} + \sum_{l \neq i} b_{il}\right) & i = k \\ -g_{ik} - \mathrm{j}b_{ik} & \text{otherwise.} \end{cases} \quad (2)$$

Power flow equations

The *power flow equations* are a non-linear system of equations that describe Kirchhoff's current and voltage laws jointly. This system of equations is written as

$$\mathbf{s} := \mathbf{p} + \mathrm{j}\mathbf{q} = \mathrm{diag}(\mathbf{u}) \underline{Y} \mathbf{u}, \quad (3)$$

where $\{\cdot\}$ is the complex conjugate, $\mathbf{u} \in \mathbb{C}^n$ are the *bus voltage phasors* and $\mathbf{Y} \in \mathbb{C}^{n \times n}$ is the admittance matrix.

Much ink has been spilled over solving these equations efficiently.

The power flow manifold

Define the *network state* in $\mathbb{R}^{4n}$ as

$$\mathbf{x} := \begin{bmatrix} \mathbf{v}^\top & \boldsymbol{\theta}^\top & \mathbf{p}^\top & \mathbf{q}^\top \end{bmatrix}^\top; \quad (4)$$

the power flow equations define a nonlinear operator $\mathcal{F} : \mathbb{R}^{4n} \rightarrow \mathbb{R}^{2n}$, where

$$\mathcal{F}(\mathbf{x}) := \begin{bmatrix} \operatorname{Re} \{ \operatorname{diag}(\mathbf{u}) \underline{\mathbf{Y}} \mathbf{u} - \mathbf{s} \} \\ \operatorname{Im} \{ \operatorname{diag}(\mathbf{u}) \underline{\mathbf{Y}} \mathbf{u} - \mathbf{s} \} \end{bmatrix} \quad (5)$$

with $\mathbf{u} := \mathbf{v} \circ \exp \{ \mathbf{j} \boldsymbol{\theta} \}$ as the voltage phasors and $\mathbf{s} := \mathbf{p} + \mathbf{j} \mathbf{q}$ as the complex power injections. The *power flow manifold* is then

$$\mathcal{M} = \left\{ \mathbf{x} \in \mathbb{R}^{4n} : \mathcal{F}(\mathbf{x}) = \mathbf{0}_{2n} \right\}. \quad (6)$$

Linearized power flow manifold

The *linear manifold tangent* to $\mathcal{M}$ at a nominal operating point $\mathbf{x}_\bullet$ is given by

$$\mathcal{M}_\bullet := \left\{ \mathbf{x} \in \mathbb{R}^{4n} : \mathbf{F}(\mathbf{x}_\bullet) (\mathbf{x} - \mathbf{x}_\bullet) = \mathbf{0}_{2n} \right\}, \quad (7)$$

where

$$\mathbf{F}(\mathbf{x}_\bullet) := \frac{\partial \mathcal{F}}{\partial \mathbf{x}}(\mathbf{x}_\bullet) = \begin{bmatrix} \frac{\partial \mathcal{F}}{\partial \mathbf{v}}(\mathbf{x}_\bullet) & \frac{\partial \mathcal{F}}{\partial \boldsymbol{\theta}}(\mathbf{x}_\bullet) & \frac{\partial \mathcal{F}}{\partial \mathbf{p}}(\mathbf{x}_\bullet) & \frac{\partial \mathcal{F}}{\partial \mathbf{q}}(\mathbf{x}_\bullet) \end{bmatrix} \quad (8a)$$

$$= \begin{bmatrix} \operatorname{Re} \left\{ \frac{\partial \mathbf{s}}{\partial \mathbf{v}}(\mathbf{u}_\bullet) \right\} & \operatorname{Re} \left\{ \frac{\partial \mathbf{s}}{\partial \boldsymbol{\theta}}(\mathbf{u}_\bullet) \right\} & -\mathbf{I}_{n \times n} & \mathbf{0}_{n \times n} \\ \operatorname{Im} \left\{ \frac{\partial \mathbf{s}}{\partial \mathbf{v}}(\mathbf{u}_\bullet) \right\} & \operatorname{Im} \left\{ \frac{\partial \mathbf{s}}{\partial \boldsymbol{\theta}}(\mathbf{u}_\bullet) \right\} & \mathbf{0}_{n \times n} & -\mathbf{I}_{n \times n} \end{bmatrix} \quad (8b)$$

$$= \begin{bmatrix} \frac{\partial \mathbf{p}}{\partial \mathbf{v}}(\mathbf{u}_\bullet) & \frac{\partial \mathbf{p}}{\partial \boldsymbol{\theta}}(\mathbf{u}_\bullet) & -\mathbf{I}_{n \times n} & \mathbf{0}_{n \times n} \\ \frac{\partial \mathbf{q}}{\partial \mathbf{v}}(\mathbf{u}_\bullet) & \frac{\partial \mathbf{q}}{\partial \boldsymbol{\theta}}(\mathbf{u}_\bullet) & \mathbf{0}_{n \times n} & -\mathbf{I}_{n \times n} \end{bmatrix}. \quad (8c)$$

Linearization of the power flow manifold [1, 2, 3]

Consider the *flat start condition* $\mathbf{u}_\star := 1 + j\mathbf{0}$, and suppose that $\omega = \mathbf{0} + j\mathbf{0}$. Then, the linear power flow manifold around $\mathbf{u}_\star$ is

$$\mathcal{M}_\star := \left\{ \mathbf{x} \in \mathbb{R}^{4n} : F(\mathbf{x}_\star)(\mathbf{x} - \mathbf{x}_\star) = \mathbf{0}_{2n} \right\}, \quad (9)$$

where

$$F(\mathbf{x}_\star) = \begin{bmatrix} \mathbf{G} & -\mathbf{B} & -\mathbf{I}_{n \times n} & \mathbf{0}_{n \times n} \\ -\mathbf{B} & -\mathbf{G} & \mathbf{0}_{n \times n} & -\mathbf{I}_{n \times n} \end{bmatrix}, \quad (10)$$

or equivalently,

$$\boxed{\mathbf{p} = \mathbf{G}\epsilon - \mathbf{B}\theta, \quad \text{and} \quad \mathbf{q} = -\mathbf{B}\epsilon - \mathbf{G}\theta,} \quad (11)$$

where $\epsilon := \mathbf{v} - 1$.

Flat start linearization, part 1

Let $\omega := \gamma + j\beta \in \mathbb{C}^n$ denote the vector of self-admittances of each node. Then, following [5, 5.10]

$$\begin{aligned}\frac{\partial \mathbf{s}}{\partial \boldsymbol{\theta}}(\mathbf{u}_\star) &= j \operatorname{diag}(\mathbf{u}_\star) (\operatorname{diag}(\underline{\mathbf{Y}} \mathbf{u}_\star) - \underline{\mathbf{Y}} \operatorname{diag}(\mathbf{u}_\star)) \\ &= j \mathbf{I}_{n \times n} (\operatorname{diag}(\underline{\mathbf{Y}} \mathbf{1}_n) - \underline{\mathbf{Y}} \mathbf{I}_{n \times n}) \\ &= j (\operatorname{diag}(\underline{\omega}) - \underline{\mathbf{Y}})\end{aligned}$$

and

$$\begin{aligned}\frac{\partial \mathbf{s}}{\partial \mathbf{v}}(\mathbf{u}_\star) &= \operatorname{diag}(\mathbf{u}) (\operatorname{diag}(\underline{\mathbf{Y}} \mathbf{u}) + \underline{\mathbf{Y}} \operatorname{diag}(\mathbf{u})) \operatorname{diag}(\mathbf{v})^{-1} \\ &= \mathbf{I}_{n \times n} (\operatorname{diag}(\underline{\mathbf{Y}} \mathbf{1}_n) + \underline{\mathbf{Y}} \mathbf{I}_{n \times n}) \mathbf{I}_{n \times n}^{-1} \\ &= \operatorname{diag}(\underline{\omega}) + \underline{\mathbf{Y}}\end{aligned}$$

Flat start linearization, part 2

We have that

$$\begin{aligned}\frac{\partial \mathbf{p}}{\partial \boldsymbol{\theta}}(\mathbf{u}_\star) &:= \operatorname{Re} \left\{ \frac{\partial \mathbf{s}}{\partial \boldsymbol{\theta}}(\mathbf{u}_\star) \right\} \\ &= \operatorname{Re} \{ \mathbf{j} (\operatorname{diag}(\boldsymbol{\omega}) - \mathbf{Y}) \} \\ &= \operatorname{Re} \{ \mathbf{j} (\operatorname{diag}(\boldsymbol{\gamma} - \mathbf{j}\boldsymbol{\beta}) - (\mathbf{G} - \mathbf{j}\mathbf{B})) \} \\ &= \operatorname{Re} \{ \mathbf{j} \operatorname{diag}(\boldsymbol{\gamma}) + \operatorname{diag}(\boldsymbol{\beta}) - \mathbf{j}\mathbf{G} - \mathbf{B} \} \\ &= \operatorname{diag}(\boldsymbol{\beta}) - \mathbf{B},\end{aligned}$$

and

$$\begin{aligned}\frac{\partial \mathbf{p}}{\partial \mathbf{v}}(\mathbf{u}_\star) &:= \operatorname{Re} \{ \operatorname{diag}(\boldsymbol{\omega}) + \mathbf{Y} \} \\ &= \operatorname{Re} \{ \operatorname{diag}(\boldsymbol{\gamma} - \mathbf{j}\boldsymbol{\beta}) + \mathbf{G} - \mathbf{j}\mathbf{B} \} \\ &= \operatorname{diag}(\boldsymbol{\gamma}) + \mathbf{G}.\end{aligned}$$

Flat start linearization, part 3

Similarly,

$$\begin{aligned}\frac{\partial \mathbf{q}}{\partial \boldsymbol{\theta}}(\mathbf{u}_\star) &= \text{Im} \left\{ \frac{\partial \mathbf{s}}{\partial \boldsymbol{\theta}}(\mathbf{u}_\star) \right\} \\ &= \text{Im} \{ \mathbf{j} (\text{diag}(\underline{\boldsymbol{\omega}}) - \underline{\mathbf{Y}}) \} \\ &= \text{Im} \{ \mathbf{j} \text{diag}(\boldsymbol{\gamma}) + \text{diag}(\boldsymbol{\beta}) - \mathbf{j}\mathbf{G} - \mathbf{B} \} \\ &= \text{diag}(\boldsymbol{\gamma}) - \mathbf{G}\end{aligned}$$

and

$$\begin{aligned}\frac{\partial \mathbf{q}}{\partial \mathbf{v}}(\mathbf{u}_\star) &= \text{Im} \{ \text{diag}(\underline{\boldsymbol{\omega}}) + \underline{\mathbf{Y}} \} \\ &= \text{Im} \{ \text{diag}(\boldsymbol{\gamma} - \mathbf{j}\boldsymbol{\beta}) + \mathbf{G} - \mathbf{j}\mathbf{B} \} \\ &= -\text{diag}(\boldsymbol{\beta}) - \mathbf{B}\end{aligned}$$

Applying the assumption that $\beta = \gamma = \mathbf{0}$ and plugging into (8) yields the desired result:

$$F(\mathbf{x}_\star) = \begin{bmatrix} \mathbf{G} & -\mathbf{B} & -\mathbf{I}_{n \times n} & \mathbf{0}_{n \times n} \\ -\mathbf{B} & -\mathbf{G} & \mathbf{0}_{n \times n} & -\mathbf{I}_{n \times n} \end{bmatrix}. \quad (12)$$

Remark: Model inversion

In the special case of *radial (tree) networks*, i.e., the practically relevant setting of small-scale *distribution networks* (the main application setting of interest), a reduced form of the linear model (11) can be inverted in closed form.

Trees only

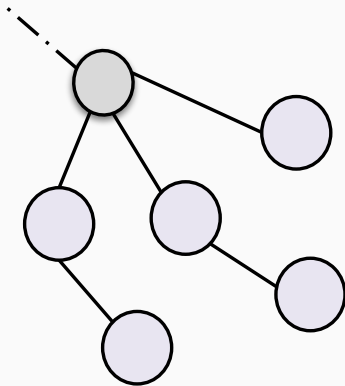


Figure 1: Hereafter, everything only works for tree networks

Reduced incidence matrix

With an abuse of notation, for a **tree network** with n lines and n non-reference nodes, $\mathcal{N} := \{0, 1, \dots, n\}$, let $\mathbf{A} \in \{0, \pm 1\}^{n \times n}$ be the reduced incidence matrix formed by removing the first column of the full incidence matrix, which we now denote as

$$\mathbf{A}_\star := \begin{bmatrix} \mathbf{a}_0 & \mathbf{A} \end{bmatrix} \in \{0, \pm 1\}^{n \times (n+1)}. \quad (13)$$

It is known that the reduced incidence matrix $\mathbf{A}$ is square and invertible [4].

Reduced Laplacian matrices

With another abuse of notation, keep the same formula for the admittance matrix Y ,

$$Y := A^T \text{diag}(\mathbf{w})A = A^T \text{diag}(\mathbf{g})A + jA^T \text{diag}(\mathbf{b})A, \quad (14)$$

and define the following reduced graph Laplacian matrices:

$$\mathbf{G} := \text{Re}\{Y\} = A^T \text{diag}(\mathbf{g})A, \quad \text{and} \quad \mathbf{B} := \text{Im}\{Y\} = A^T \text{diag}(\mathbf{b})A, \quad (15)$$

where A is now the *reduced incidence matrix*.

Now the inverse of Y , the *impedance matrix*, can be computed as

$$Y^{-1} = A^{-1} \text{diag}(\mathbf{w})^{-1} A^{-T} = R + jX. \quad (16)$$

Intuitive explanation

Recall that for any complex number ζ , $\zeta^{-1} = \underline{\zeta} / |\zeta|^2$. Hence, the impedances can be expressed as inverse admittances (graph weights):

$$w_{ij}^{-1} := r_{ij} + jx_{ij} := \underbrace{\frac{g_{ij}}{g_{ij}^2 + b_{ij}^2}}_{:=r_{ij}} + j \underbrace{\frac{-b_{ij}}{g_{ij}^2 + b_{ij}^2}}_{:=x_{ij}} \quad \forall (i, j) \in \mathcal{E}, \quad (17)$$

thus, define the matrices

$$R = A^{-1} \text{diag}(r) A^{-T}, \quad X := A^{-1} \text{diag}(x) A^{-T}.$$

Inverse model for tree networks

Consider a tree network with n non-reference nodes and n edges. Then,

$$\begin{bmatrix} G & -B \\ -B & -G \end{bmatrix}^{-1} = \begin{bmatrix} R & X \\ X & -R \end{bmatrix}, \quad (18)$$

where

$$R = A^{-1} \text{diag}(r) A^{-\top},$$
$$X := A^{-1} \text{diag}(x) A^{-\top}.$$

and thus

$$\boxed{\epsilon = Rp + Xq, \quad \text{and} \quad \theta = Xp - Rq,} \quad (19)$$

where $\epsilon := v - 1$.

Inverting the model for trees

We want to invert the system of equations

$$\begin{bmatrix} p \\ q \end{bmatrix} = \begin{bmatrix} G & -B \\ -B & -G \end{bmatrix} \begin{bmatrix} \epsilon \\ \theta \end{bmatrix}. \quad (20)$$

Note that as $G \succ 0$, both Schur complements of the above matrix exist, and hence

$$\begin{aligned} \begin{bmatrix} G & -B \\ -B & -G \end{bmatrix}^{-1} &= \begin{bmatrix} (G + BG^{-1}B)^{-1} & 0_{n \times n} \\ 0_{n \times n} & - (G + BG^{-1}B)^{-1} \end{bmatrix} \begin{bmatrix} I_{n \times n} & -BG^{-1} \\ BG^{-1} & I_{n \times n} \end{bmatrix} \\ &= \begin{bmatrix} (G + BG^{-1}B)^{-1} & - (G + BG^{-1}B)^{-1} BG^{-1} \\ - (G + BG^{-1}B)^{-1} BG^{-1} & - (G + BG^{-1}B)^{-1} \end{bmatrix}. \end{aligned}$$

Inverting the model for trees

To begin, the first matrix we need to compute is

$$\begin{aligned} \left(\mathbf{G} + \mathbf{B}\mathbf{G}^{-1}\mathbf{B} \right)^{-1} &= \left(\mathbf{A}^T \text{diag}(\mathbf{g})\mathbf{A} + \mathbf{A}^T \text{diag}(\mathbf{b})\mathbf{A}\mathbf{A}^{-1} \text{diag}(\mathbf{g})^{-1}\mathbf{A}^{-T}\mathbf{A}^T \text{diag}(\mathbf{b})\mathbf{A} \right)^{-1} \\ &= \left(\mathbf{A}^T \text{diag} \left(\left[\frac{g_{ij}^2 + b_{ij}^2}{g_{ij}} \right]_{ij \in \mathcal{E}} \right) \mathbf{A} \right)^{-1} \\ &= \mathbf{A}^{-1} \text{diag} \left(\left[\frac{g_{ij}}{g_{ij}^2 + b_{ij}^2} \right]_{ij \in \mathcal{E}} \right) \mathbf{A}^{-T} \\ &:= \mathbf{A}^{-1} \text{diag}(\mathbf{r}) \mathbf{A}^{-T} \\ &:= \mathbf{R}. \end{aligned}$$

Inverting the model for trees

Finally, the second matrix we need to compute is

$$\begin{aligned} -\left(\mathbf{G} + \mathbf{B}\mathbf{G}^{-1}\mathbf{B}\right)^{-1}\mathbf{B}\mathbf{G}^{-1} &= -\mathbf{A}^{-1}\text{diag}\left(\left[\frac{g_{ij}}{g_{ij}^2 + b_{ij}^2}\right]_{ij \in \mathcal{E}}\right)\mathbf{A}^{-\top}\mathbf{A}^{\top}\text{diag}(\mathbf{b})\mathbf{A}\mathbf{A}^{-1}\text{diag}(\mathbf{g})^{-1}\mathbf{A}^{-\top} \\ &= \mathbf{A}^{-1}\text{diag}\left(\left[\frac{-b_{ij}}{g_{ij}^2 + b_{ij}^2}\right]_{ij \in \mathcal{E}}\right)\mathbf{A}^{-\top} \\ &:= \mathbf{A}^{-1}\text{diag}(\mathbf{x})\mathbf{A}^{-\top} \\ &:= \mathbf{X} \end{aligned}$$

The matrices of the inverted model

Then, the matrix inverse we have obtained is

$$\begin{bmatrix} G & -B \\ -B & -G \end{bmatrix}^{-1} = \begin{bmatrix} R & X \\ X & -R \end{bmatrix} \quad (21)$$

and thus

$$\begin{bmatrix} \epsilon \\ \theta \end{bmatrix} = \begin{bmatrix} R & X \\ X & -R \end{bmatrix} \begin{bmatrix} p \\ q \end{bmatrix}, \quad (22)$$

as desired.

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